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5G Technology Workshop during Mobile World Congress in Barcelona

Dimensionality Reduction Techniques for Digital Predistortion Linearization of NR- 5G Amplification Architectures

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- ❑ Introduction
- ❑ Linearity vs. Efficiency Trade-off
- ❑ High Efficient Amplification Architectures
- ❑ Digital Predistortion (DPD) Linearization
- ❑ Dimensionality Reduction Techniques
- ❑ Conclusion

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Source: <https://www.thegigcartel.com/News/mobile-phones-banned-at-two-london-eventim-apollo-gigs.htm>

- Increasing demand of data traffic →
 - Spectrally efficient modulation schemes required + CA + MIMO
 - Wide bandwidths and high PAPRs signals

- ❑ In 5G-NR the **same network infrastructure** will be able to efficiently serve **different types of traffic** with a very wide range of requirements:
 - huge number of users for the **Internet of Things**,
 - ultra-low latency and high reliability for **mission critical systems**,
 - or enhanced transmission rates for broadband **mobile communications**.

- ❑ 5G-NR intends to provide **very high data rates** everywhere:
 - Bandwidths up to **GHz** will be allocated at **mm-wave**.
 - Aggregated bandwidths of **hundreds of MHz** will be required at **sub-6 GHz**.

For the **design of radio transceivers**, some of the demanding challenges that needs to be faced are related to:

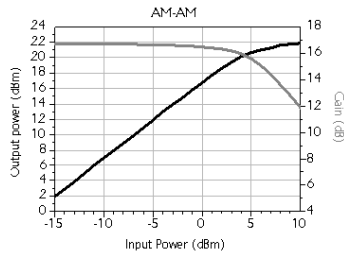
- ensuring the **linearity of signals** having bandwidths of several hundreds of MHz and peak factors exceeding 10 dB,
- improving **energy and computational efficiency**, as more dense deployments of base stations is expected to scale down the need for transmitted power,
- transmitting architectures with **multiple antennas** (massive MIMO in mm-wave bands) and multiple power amplifiers to apply beamforming techniques that allow increasing the capacity and decreasing the radiated power,
- **simultaneous transmission and reception** (full-duplex FDD in sub 6 GHz bands, TDD in mm-wave bands).

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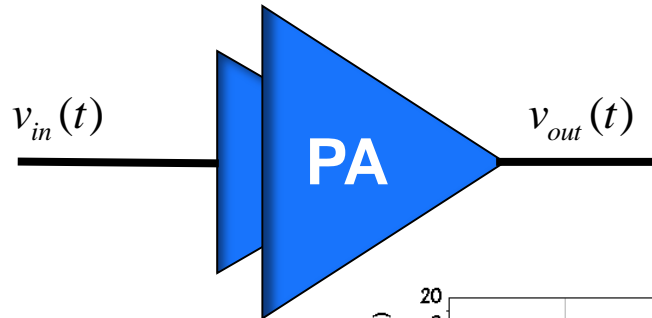
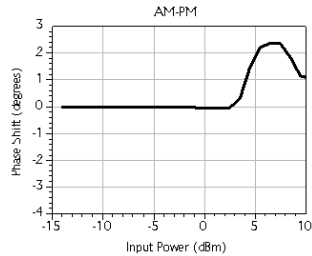
Linearity vs. Efficiency

The Power Amplifier is a power hungry device...

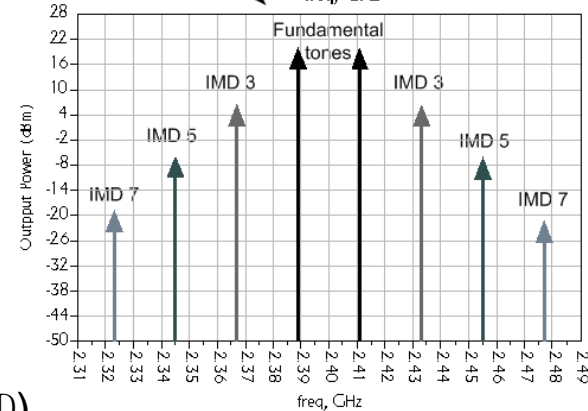
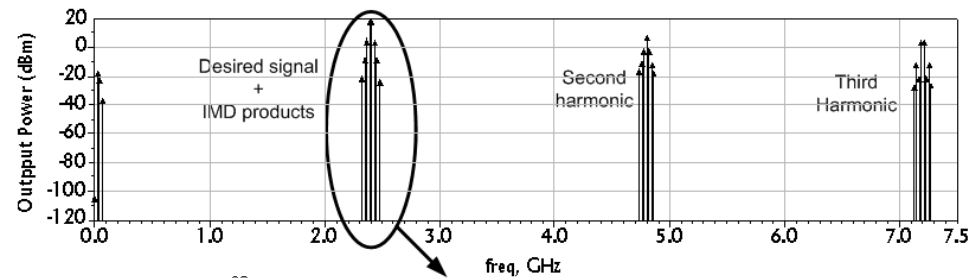
AM-AM



AM-PM



$$v_{out}(t) \approx \sum_{k=1}^{\infty} g_k v_{in}^k(t)$$



In-Band Distortion

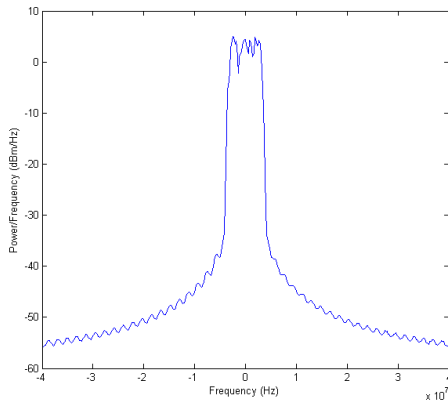
- Compression
- Capture

Out-of-Band Distortion

- Harmonic Distortion (HD)
- Intermodulation Distortion (IMD)

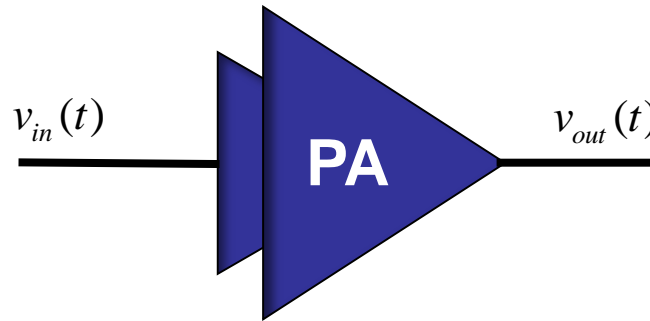
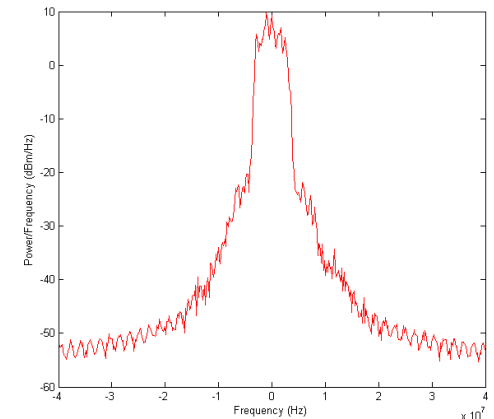
Linearity vs. Efficiency

...that introduces unwanted nonlinear distortion...



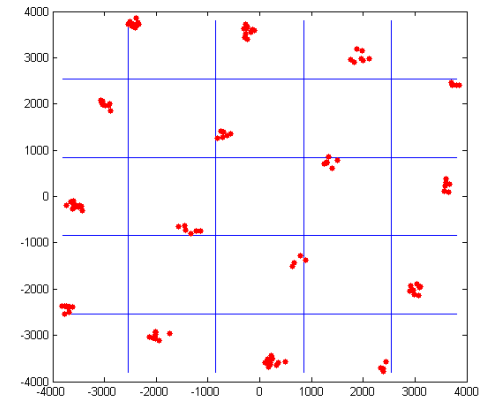
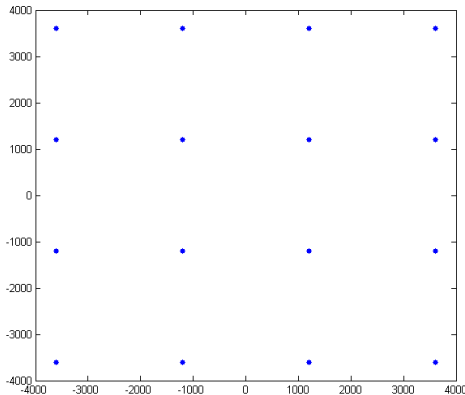
Out-of-band Distortion

$$ACPR = \frac{\int_B P_{out}(f) \cdot df}{\int_{LS} P_{out}(f) \cdot df + \int_{US} P_{out}(f) \cdot df} \quad [dBc]$$



In-band Distortion

$$EVM = \sqrt{\frac{\frac{1}{N} \sum_1^N (\Delta I^2 + \Delta Q^2)}{S_{max}^2}} \quad [\%]$$

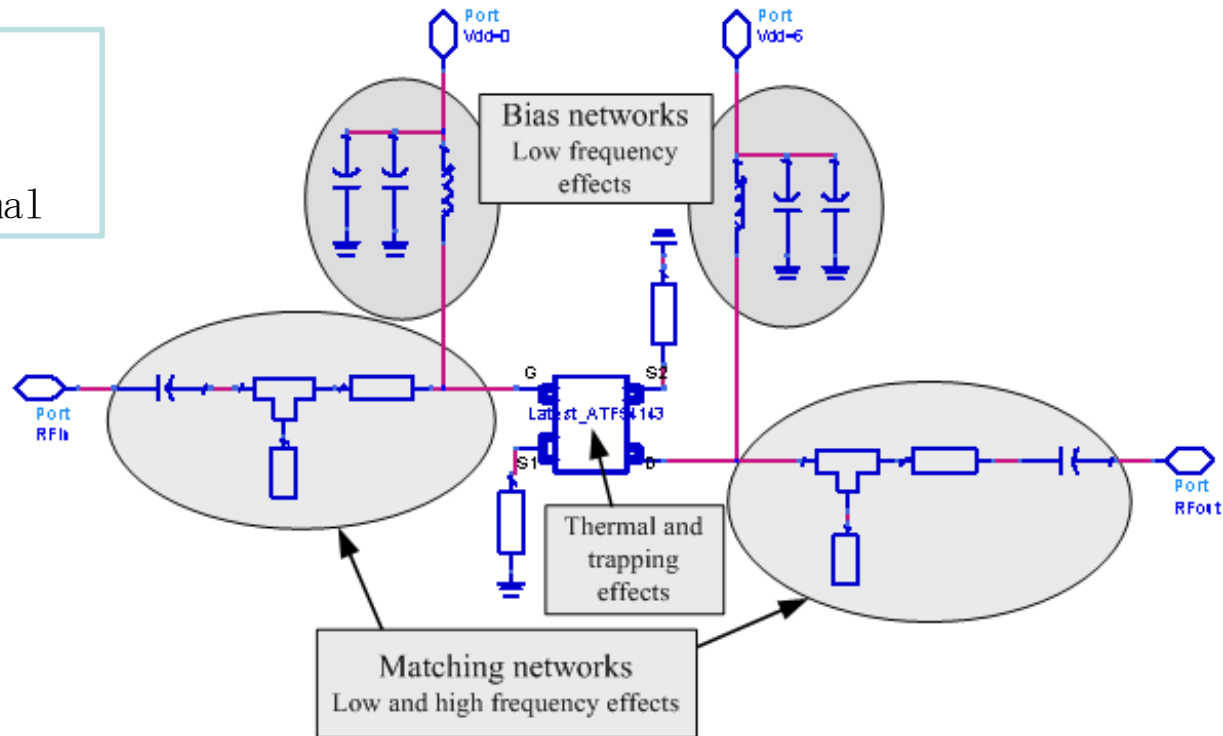


...and linear distortion (memory effects)...

Main sources of memory effects in PAs

Main types:

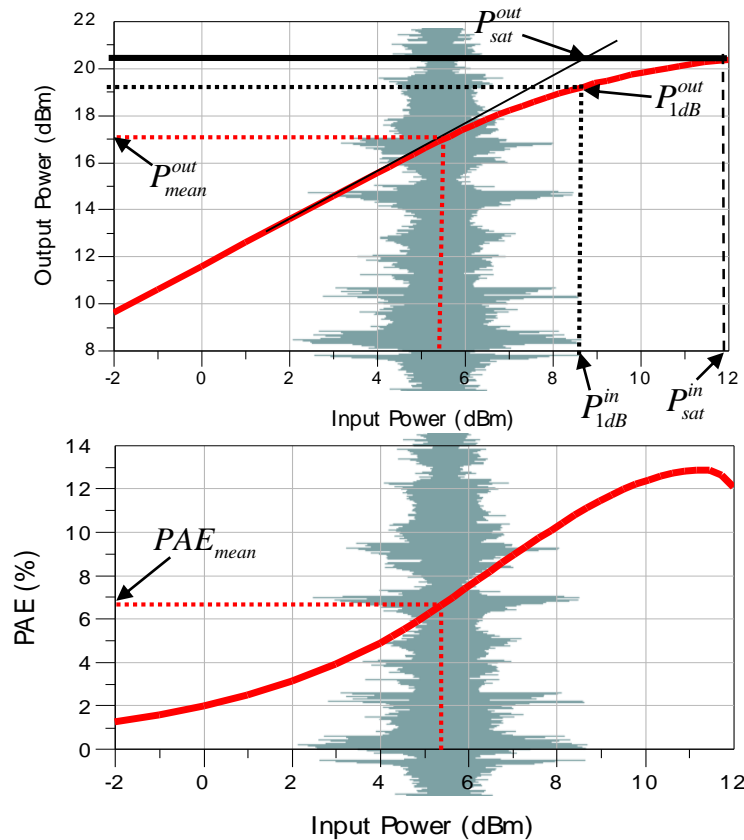
- Electrical
- Electrothermal



□ They appear as:

- Asymmetries in the IMD products (frequency domain)
- Dispersion in the decision points of the constellation (time domain)

Back-off operation results power inefficient (class A, class AB below 20% with PAPR up to 9dB). The more efficient is the PA class of operation the more nonlinear it results.




- 2G → GMSK → PAPR=0dB. With constant envelope modulated signals → class-C PAs → drain efficiency around 65%.
- 3G/4G/5G → non-constant envelope modulated signals:
 - WCDMA → PAPR=10.6 dB;
 - OFDM-based → PAPR~12 dB;

Modulations designed to maximize spectral efficiency, not power efficiency!

PAPR or Crest Factor Reduction (CFR) techniques for multicarrier signals

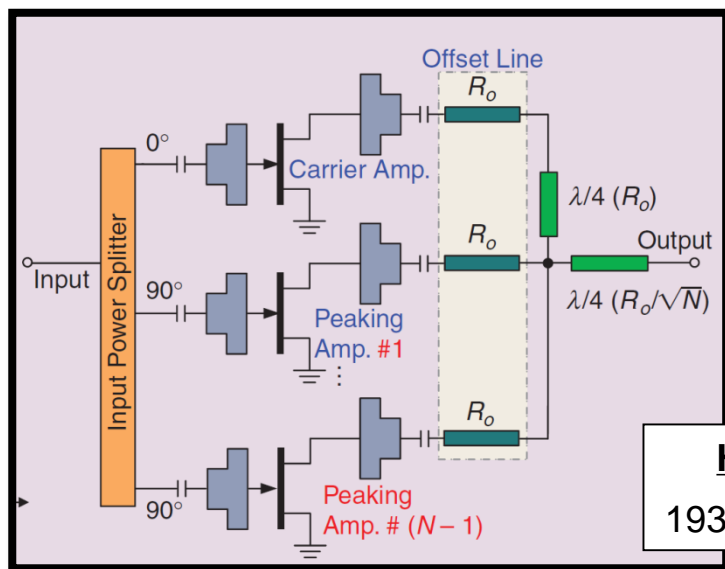
	Distortionless	Power increase	Data rate loss	Requires processing at transmitter (Tx) and receiver (Rx)
Clipping and filtering	No	No	No	Tx: Amplitude clipping, filtering Rx: None
Coding	Yes	No	Yes	Tx: Encoding or table search Rx: Decoding or table search
PTS	Yes	No	Yes	Tx: M IDFTs, W^{M-1} complex vector sums Rx: Side information extraction, inverse PTS
SLM	Yes	No	Yes	Tx: U IDFTs Rx: Side information extraction, inverse SLM
Interleaving	Yes	No	Yes	Tx: K IDFTs, $(K - 1)$ interleavings Rx: Side information extraction, inverse interleaving
TR	Yes	Yes	Yes	Tx: IDFTs, find value of PRCs Rx: Ignore non-data-bearing subcarriers
TI	Yes	Yes	No	Tx: IDFTs, search for maximum point in time, tones to be modified, value of p and q Rx: Modulo- D operation
ACE	Yes	Yes	No	Tx: IDFTs, projection onto "shaded area" Rx: None

 Seung Hee Han and Jae Hong Lee, "An overview of peak-to-average power ratio reduction techniques for multicarrier transmission," in *IEEE Wireless Communications*, vol. 12, no. 2, pp. 56-65, April 2005.

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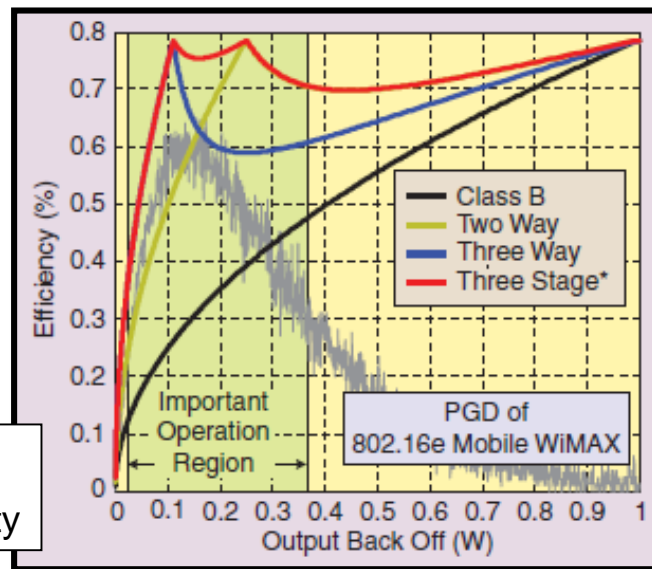
- Alternative amplification architectures/topologies to the conventional Cartesian Tx with linear class AB PA to achieve high power efficiency with the high PAPR waveforms.
 - **Dynamic Load Modulation** (Doherty PAs, Outphasing techniques)
 - **Dynamic Supply Techniques** (ET/ Class G PAs)
 - **All-digital Tx**
- **Crest Factor Reduction** (CFR) techniques to control PAPR.
- High efficient topologies demand **linearization techniques** to guarantee the linearity levels (i.e., ACLR, NMSE, EVM).

Doherty Power Amplifier



N-way Doherty PA

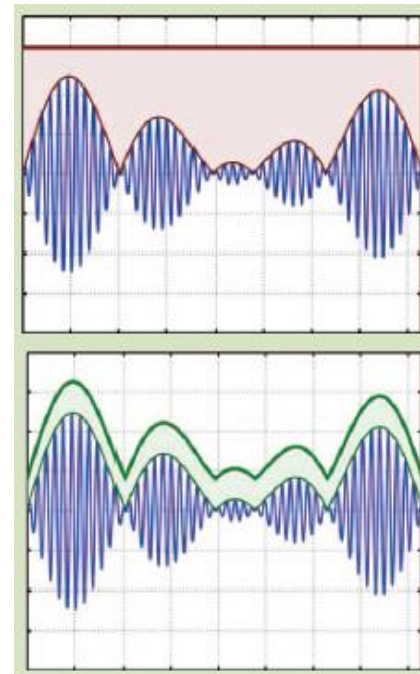
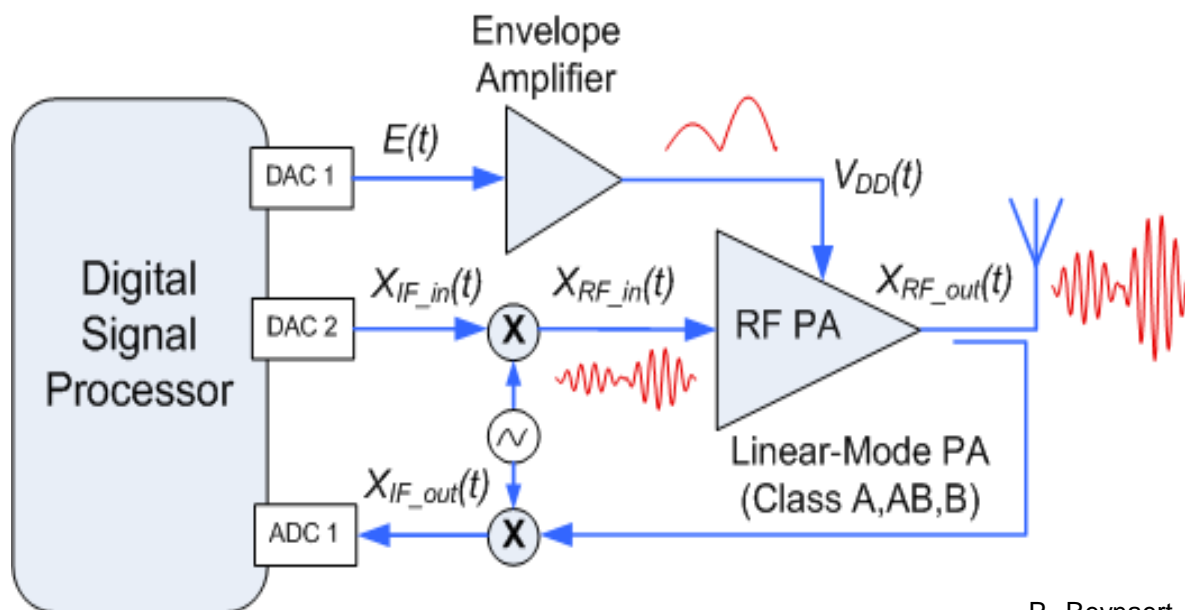
HISTORY:
1936 W. Doherty



Efficiency of different Doherty and class B PAs

The Doherty configuration uses separate carrier and peaking PAs. Only the carrier PA is turned on during low-power operation, while the two PAs are turned on at high power → high efficiency at backed-off output power level as well as at the peak power.

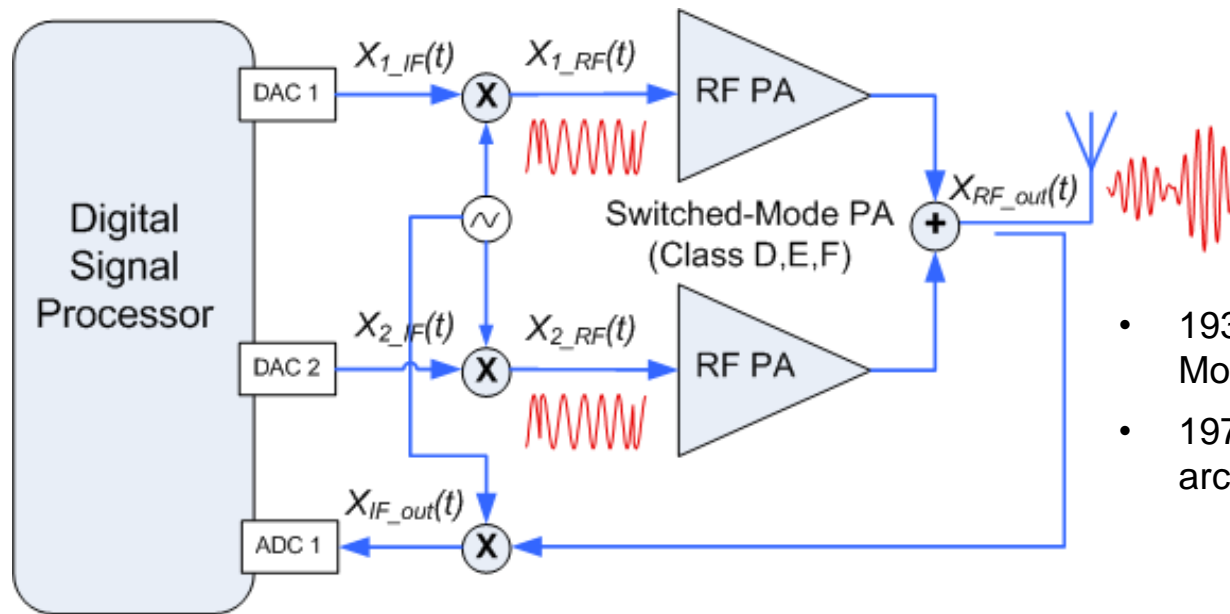
Envelope Tracking



P. Reynaert, "Polar Modulation," *IEEE Microwave Magazine*, vol. 12, pp. 46-51, Feb. 2011.

The supply voltage of the RF PA is adjusted according to the envelope of the RF carrier. Thanks to the **dynamic supply** the RF PA is always operating close to saturation which increases the power efficiency at power back-off.

LINC or Outphasing PAs

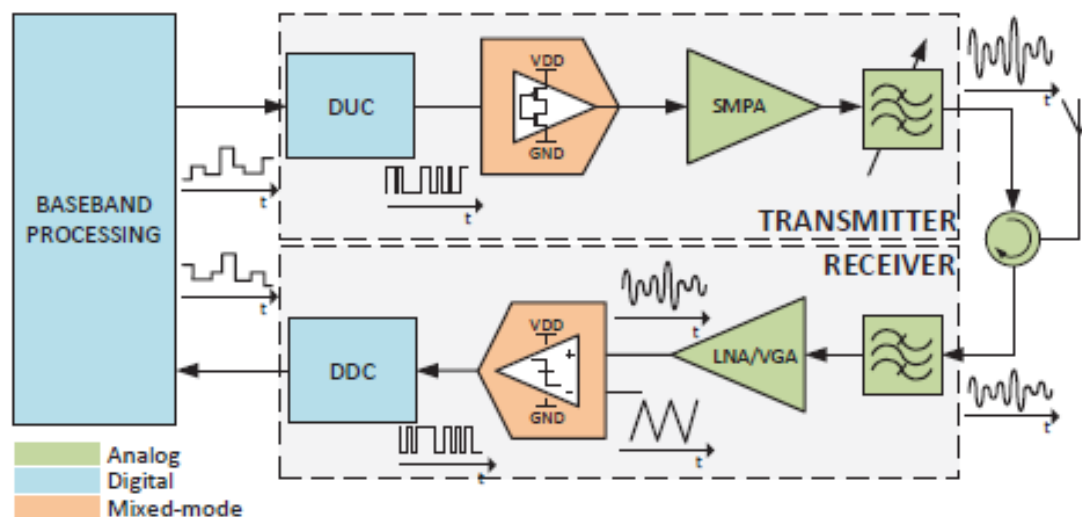



HISTORY

- 1935, H. Chireix - Outphasing Mod. Arrangement
- 1974, D.C. Cox - LINC architecture

The input signal is converted into **two constant envelope signals**. These two signals are amplified independently by two high-efficient switched-mode PAs in parallel branches. At the PA outputs, both signals are added in a two-to-one combiner obtaining a linear amplified replica of the input.

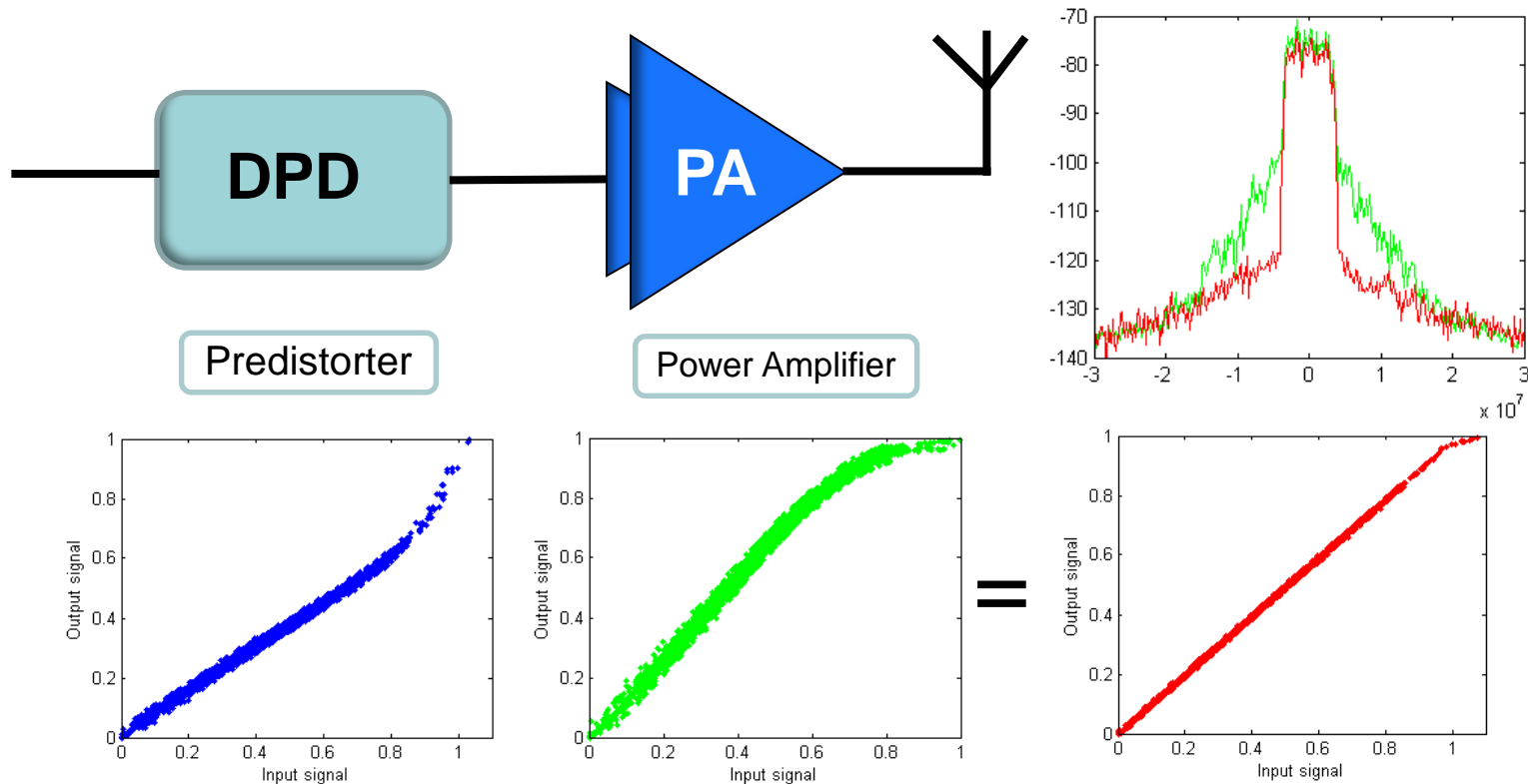
All-digital Transmitters

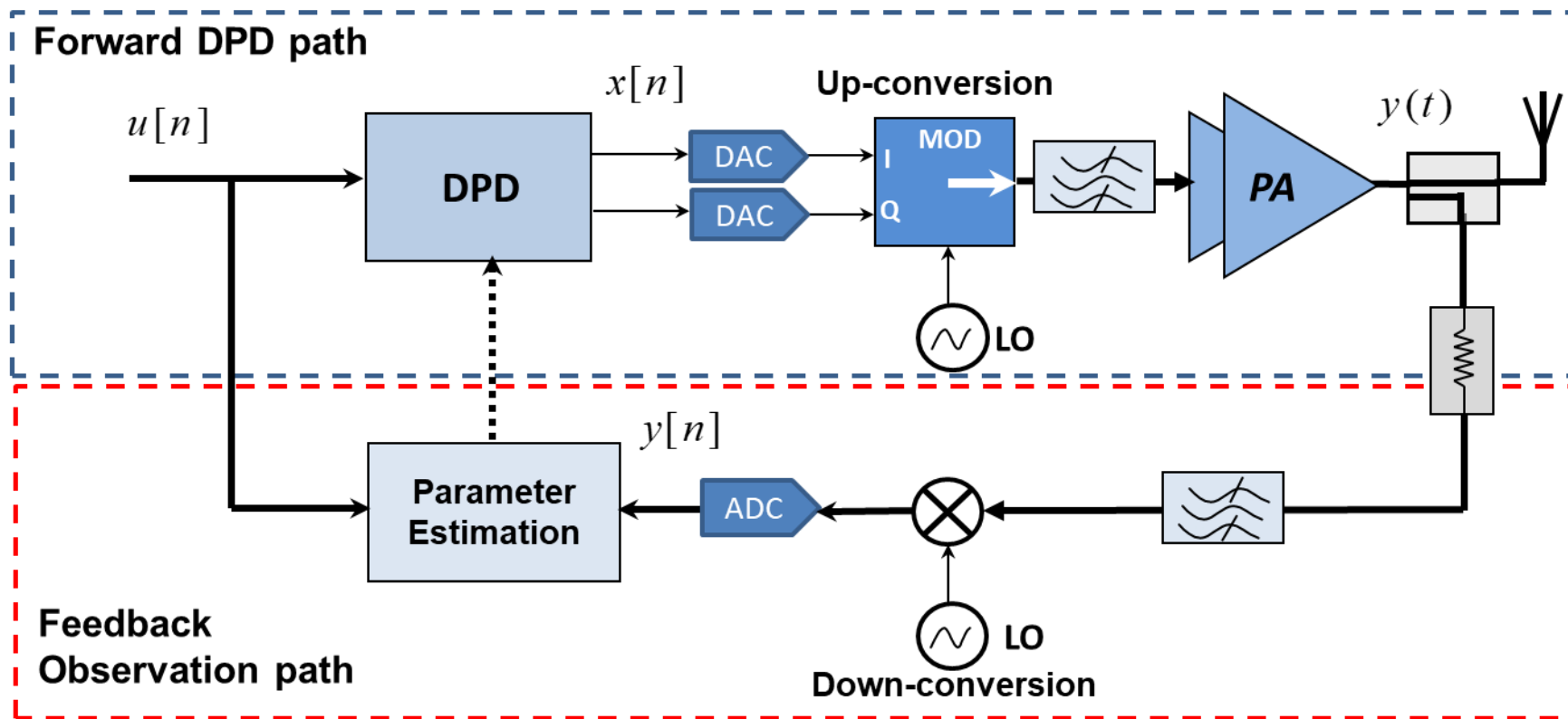


 A. Prata, R. F. Cordeiro, D. C. Dinis, S. R. Oliveira, J. Viera and N. B. Carvalho, "All-Digital Transceivers – Recent Advances and Trends," in Proc IEEE International Conf. on Electronics, Circuits and Integrated Systems - ICECS, Monte Carlo, Monaco, Vol., pp. - , December, 2016.

In all-digital Tx. architectures, **pulse width or delta-sigma modulators** convert the signal from multi-level to 2-level. The pulsed digital RF signal is converted to the analog domain with a high-speed digital buffer and a **2-level Switched-Mode PA**. The analog output **reconstruction filter** removes the quantization noise.

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SISO DPD


Memory Polynomial

$$\hat{y}[n] = \sum_{i=0}^N \sum_{p=0}^P \gamma_{pi} \cdot x[n - \tau_i] \cdot |x[n - \tau_i]|^p$$

 J. Kim, K. Konstantinou, "Digital predistortion of wideband signals based on power amplifier model with memory", Electronics Letters, vol. 37, n. 23, pp: 1417-1418, Nov. 2001

Nonlinear Auto-Regressive Moving Average (NARMA)


$$\hat{y}[n] = \sum_{i=0}^N \sum_{p=0}^P \alpha_{pi} \cdot x[n - \tau_i^N] \cdot |x[n - \tau_i^N]|^p - \sum_{j=1}^D \sum_{q=0}^Q \beta_{qj} \cdot \hat{y}[n - \tau_j^D] \cdot |\hat{y}[n - \tau_j^D]|^q$$

 G. Montoro et al. "A New Digital Predictive Predistorter for Behavioral Power Amplifier Linearization," IEEE Microwave and Wireless Components Letters, vol. 17, pp. 448-450, June 2007.

Generalized Memory Polynomial

$$\hat{y}[n] = \sum_{l=0}^{L_A} \sum_{p=0}^{P_A} a_{pl} \cdot x[n - \tau_l^A] \cdot |x[n - \tau_l^A]|^p + \sum_{l=1}^{L_B} \sum_{m=1}^{M_B} \sum_{p=0}^{P_B} b_{pml} \cdot x[n - \tau_l^B] \cdot |x[n - \tau_l^B - \tau_m^B]|^p$$

$$+ \sum_{l=1}^{L_C} \sum_{m=1}^{M_C} \sum_{p=0}^{P_C} c_{pml} \cdot x[n - \tau_l^C] \cdot |x[n - \tau_l^C + \tau_m^C]|^p$$

 D. R. Morgan, Z. Ma, J. Kim, M. G. Zierdt, and J. Pastalan, "A Generalized Memory Polynomial Model for Digital Predistortion of RF Power Amplifiers," IEEE Trans. on Signal Proc., vol 54, pp. 3852-3860, Oct. 2006.


SISO DPD

Volterra Series


$$\hat{y}[n] = \sum_{k=1}^R \sum_{q_k=0}^{Q_k-1} \dots \sum_{q_1=0}^{Q_1-1} h_k(q_1, \dots, q_k) \prod_{i=1}^k x[n - \tau_{q_i}]$$

Variations of Volterra series:


- **Dynamic Deviation Reduction Volterra Series**


 A. Zhu, J. Pedro and T. Brazil, "Dynamic Deviation Reduction-Based Volterra Behavioral Modeling of RF Power Amplifiers," IEEE Transactions on Microwave Theory and Techniques, vol. 54, no. 12, pp. 4323-4332, December 2006.

- **Volterra Behavioral Model for Wideband PAs (VBW)**

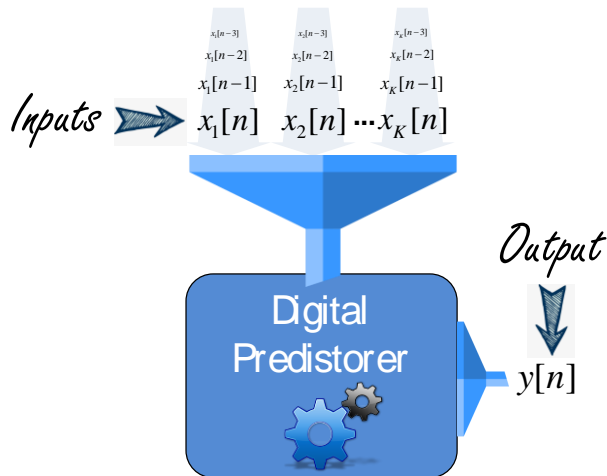
 C. Crespo-Cadenas, J. Reina-Tosina and M. J. Madero-Ayora, "Volterra behavioral model for wideband RF amplifiers," IEEE Transactions on Microwave Theory and Technology, vol. 55, no. 3, p. 449-457, 2007.

- **Multi-band Volterra series**

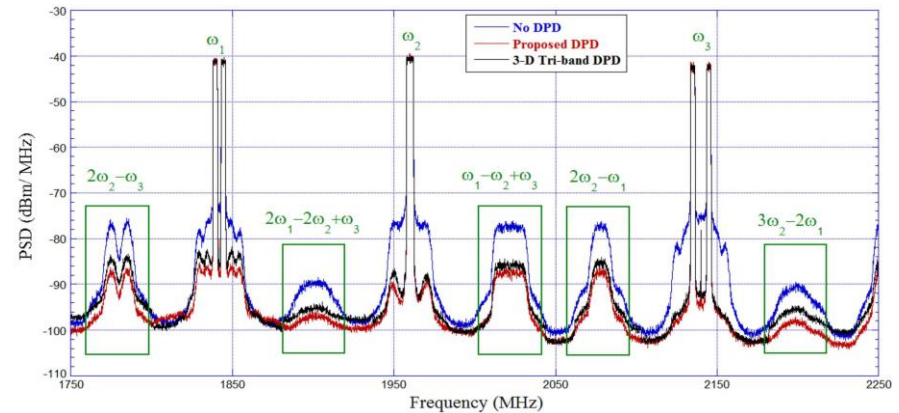
 M. Younes, A. Kwan, M. Rawat and F. M. Ghannouchi, "Linearization of Concurrent Tri-Band Transmitters Using 3-D Phase-Aligned Pruned Volterra Model," in IEEE Transactions on Microwave Theory and Techniques, vol. 61, no. 12, pp. 4569-4578, Dec. 2013.

 J. Kim, P. Roblin, D. Chaillot, and X. Zhijian, "A generalized architecture for the frequency-selective digital predistortion linearization technique," IEEE Transactions on Microwave Theory and Techniques, vol. 61, no. 1, pp. 596-605, 2013.

MISO DPD

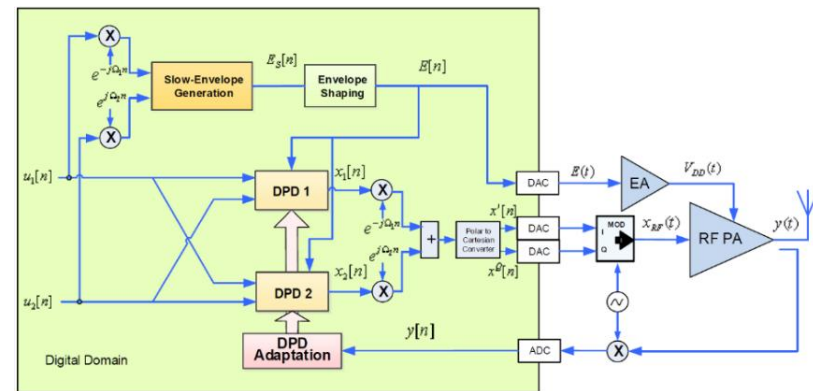
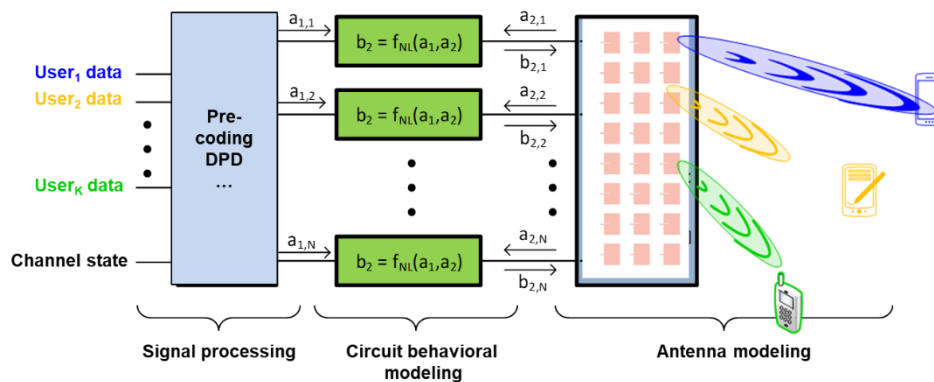


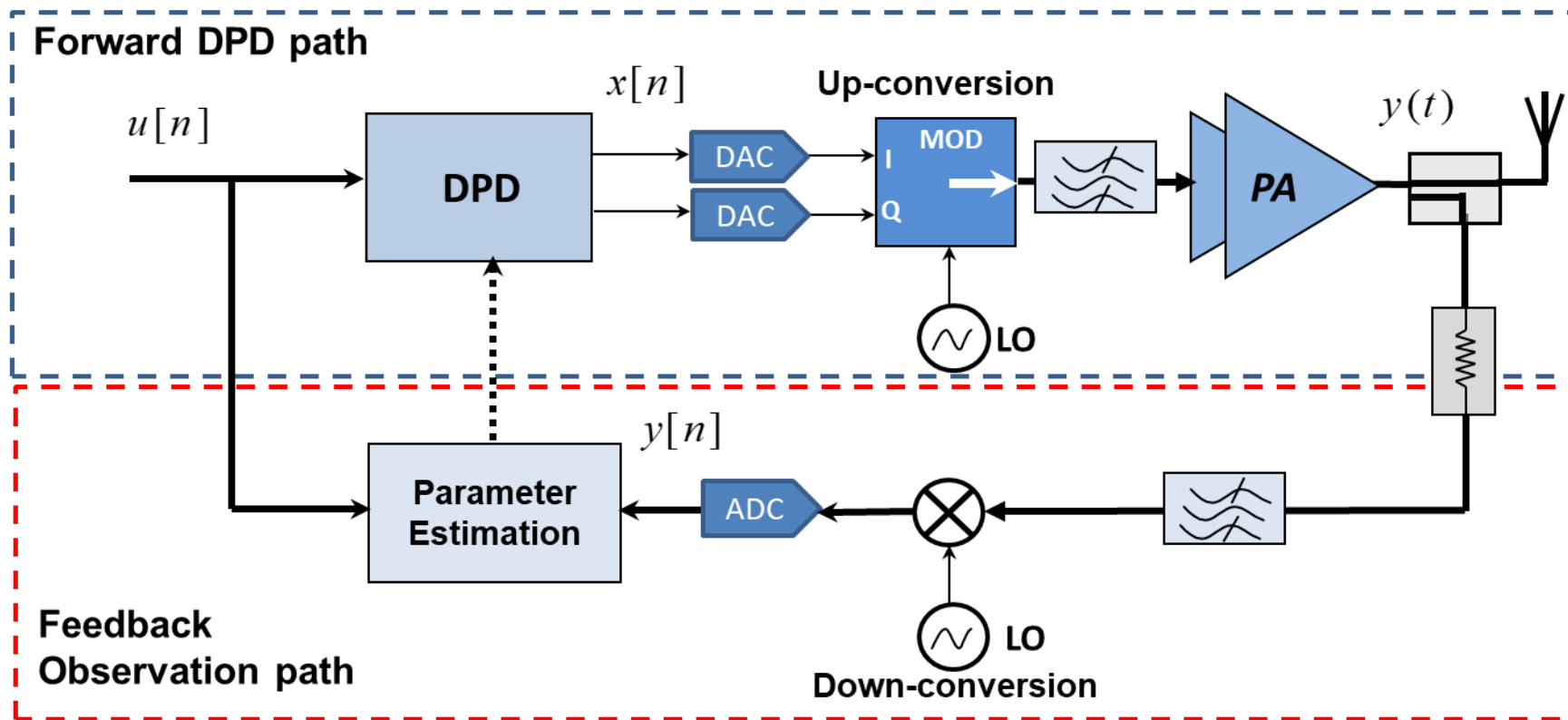
For Concurrent Multi-Band TX.



For Envelope Tracking/Outphasing PAs

For MIMO TXs





Direct Learning DPD

$$x[n] = u[n] - \boldsymbol{\varphi}_n \mathbf{w}$$

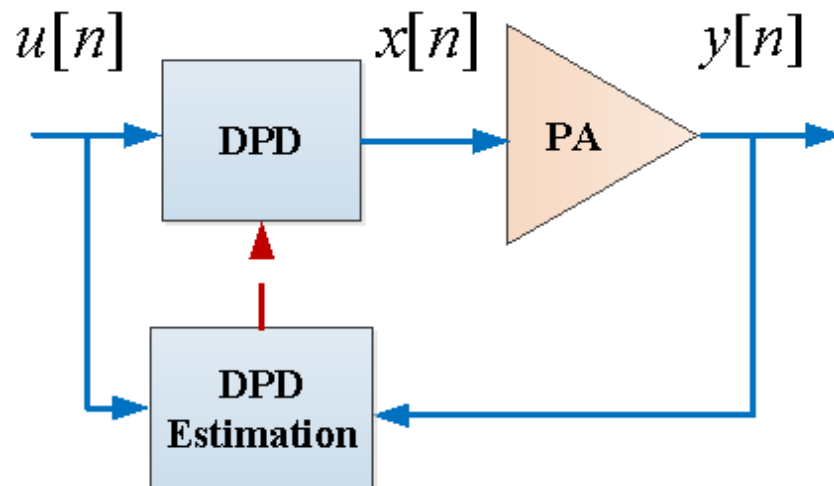
$$\mathbf{w}^{i+1} = \mathbf{w}^i + \mu (\mathbf{U}^H \mathbf{U})^{-1} \mathbf{U}^H \mathbf{e}$$

$$e[n] = y[n]/G_0 - u[n]$$

$$\mathbf{U} = (\boldsymbol{\varphi}_0, \boldsymbol{\varphi}_1, \dots, \boldsymbol{\varphi}_{L-1})^T \quad L \times M \text{ data matrix } (n=0, 1, \dots, L-1)$$

$$\boldsymbol{\varphi}_n = (\varphi_0[n], \varphi_1[n], \dots, \varphi_{M-1}[n]) \quad 1 \times M \text{ data vector containing the basis functions}$$

$$\mathbf{w} = (w_0, w_1, \dots, w_{M-1})^T \quad M \times 1 \text{ vector of coefficients}$$



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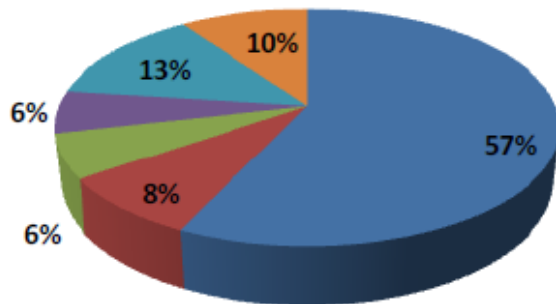
Dimens. Reduction for DPD

- In **macro BSs** it is mainly the **PA** that dominates the total power consumption



Macro

■ PA
 ■ Main Supply
 ■ DC-DC
 ■ RF
 ■ BB
 ■ Cooling

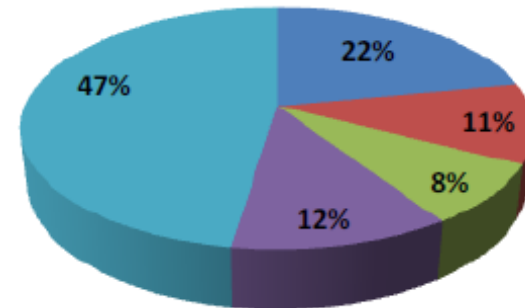


- While in **smaller BSs** it is the **baseband part** that dominates the overall power consumption

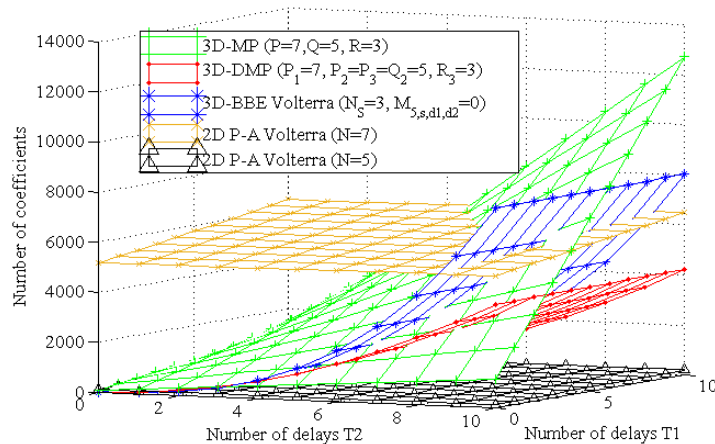


Femto/Home

■ PA
 ■ Main Supply
 ■ DC-DC
 ■ RF
 ■ BB



Considering wide bandwidth signals, carrier aggregation, concurrent multi-band transmissions, MIMO TXs \rightarrow the number of required DPD coefficients grow significantly.

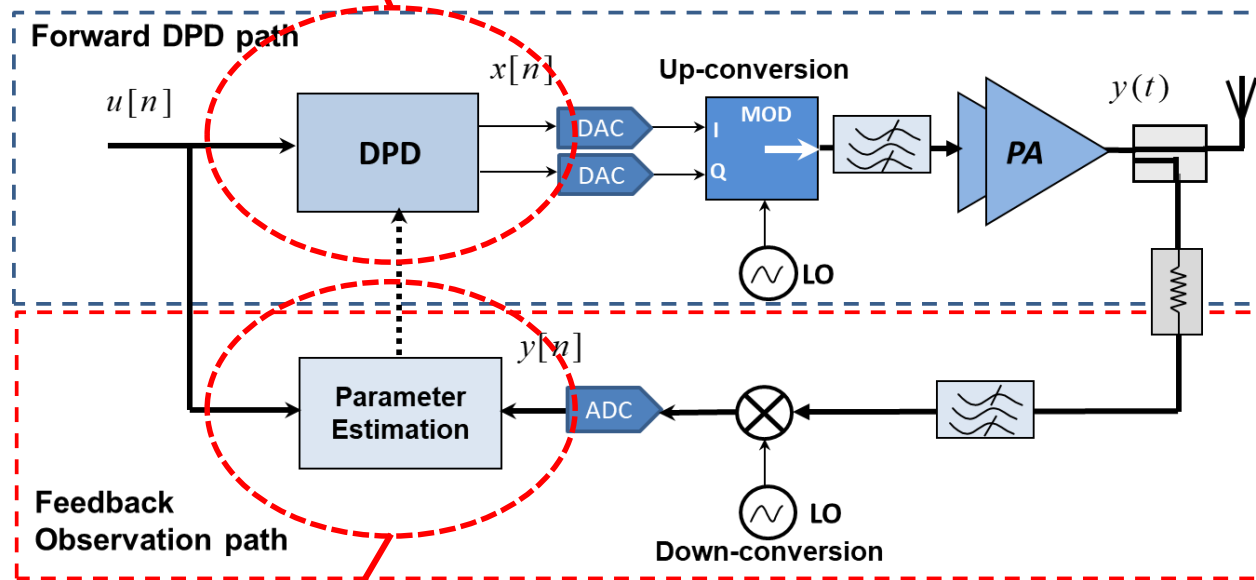


Model order reduction techniques can be applied to:

- reduce the computational complexity \rightarrow reduce baseband processing power consumption.
- improve the conditioning of the data matrices in the identification procedure (critical with high number of parameters/basis functions).

Feature Selection Techniques:

- LASSO (l1-norm regularization)
- Ridge Regression (l2-norm regularization)
- Sparse Bayesian learning (SBL) alg.
- Orthogonal Matching Pursuit (OMP) alg.
- etc.



Feature Extraction Techniques:

- Principal Component Analysis (PCA)
- Partial Least Squares (PLS)
- Canonical Correlation Analysis (CCA)
- etc.

The **sparsity of the behavioral model basis functions** can be exploited to obtain an ordered sequence of the most significant components.

$$\begin{aligned} \min_{\mathbf{w}} \quad & \|\mathbf{w}\|_0 \\ \text{subject to} \quad & \|\mathbf{y} - \mathbf{U}\mathbf{w}\|_2^2 \leq \varepsilon \end{aligned}$$

non-deterministic polynomial-
time hard (NP-hard) problem

The solution is obtained by **minimizing the number of active components** (l₀-norm) subject to a constraint on the l₂-norm squared of the identification error.

Feature Selection: Orthogonal Matching Pursuit (OMP)

1. Initialization

$$\mathbf{e}^{(0)} = \mathbf{y} - \hat{\mathbf{y}}^{(0)}; \quad \hat{\mathbf{y}}^{(0)} = \mathbf{0};$$

$$\mathcal{S}^{(0)} = \{ \}; \quad \mathcal{S}^{(n)} \equiv \text{support set containing the indices of the active coefficients of the model}$$

2. for $n=1:1:n_{\max}$

$$2.1 \quad i^{(n)} = \arg \min_i \left\{ \min_{\mathbf{w}_i} \left\| \mathbf{e}^{(n-1)} - \mathbf{U}_{\{i\}} \mathbf{w}_i \right\|_2^2 \right\} \approx \arg \max_i \left\{ \left| \mathbf{U}_{\{i\}}^H \mathbf{e}^{(n-1)} \right| \right\}$$

$$2.2 \quad \mathcal{S}^{(n)} = \mathcal{S}^{(n-1)} \cup i^{(n)}$$

$$2.3 \quad \mathbf{w}^{(n)} = \left(\mathbf{U}_{\mathcal{S}^{(n)}}^H \mathbf{U}_{\mathcal{S}^{(n)}} \right)^{-1} \mathbf{U}_{\mathcal{S}^{(n)}}^H \mathbf{y}$$

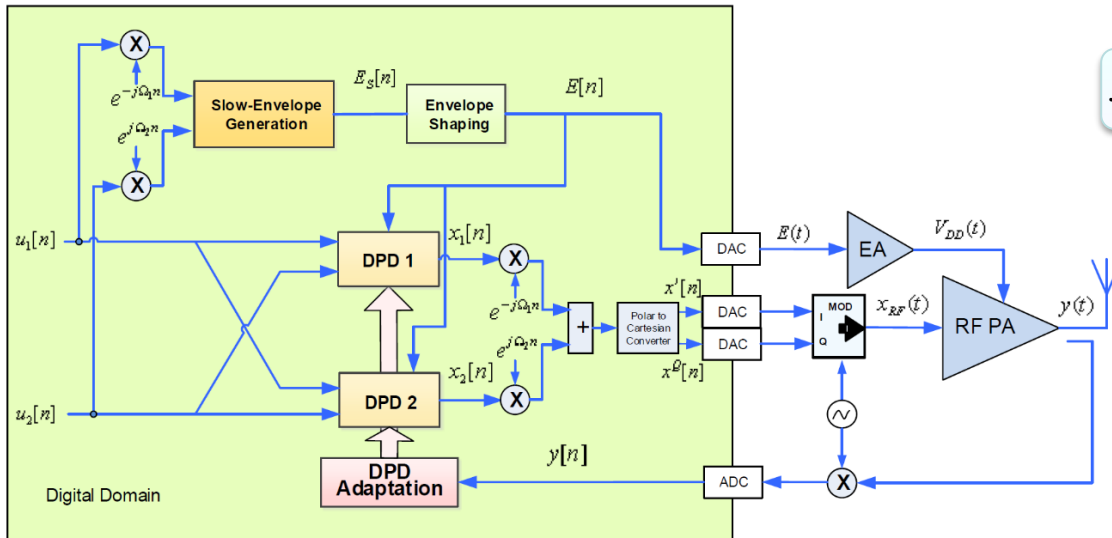
$$2.4 \quad \hat{\mathbf{y}}^{(n)} = \mathbf{U}_{\mathcal{S}^{(n)}} \mathbf{w}^{(n)}$$

$$2.5 \quad \mathbf{e}^{(n)} = \mathbf{y} - \hat{\mathbf{y}}^{(n)}$$

end

 J. Reina-Tosina, M. Allegue-Martinez, et al., "Behavioral Modeling and Predistortion of Power Amplifiers Under Sparsity Hypothesis," in IEEE Trans. on Microw. Theory and Tech., vol.63, n^o.2, pp.745-753, Feb. 2015

3D-DPD for Concurrent Dual-Band Envelope Tracking PAs



$$x[n] = f_{DPD}(u_1[n], u_2[n], E_s[n])$$

Q. A. Pham, D. Lopez-Bueno, T. Wang, G. Montoro and P. L. Gilibert, "Multi-dimensional LUT-based digital predistorter for concurrent dual-band envelope tracking power amplifier linearization," 2018 IEEE Topical Conference on RF/Microwave Power Amplifiers for Radio and Wireless Applications (PAWR), Anaheim, CA, 2018, pp. 47-50.

$$x_1[n] = \sum_{i=0}^{N_1-1} u_1[n - \tau_i^{u_1}] f_{\Phi_{1,i}}(|u_1[n - \tau_i^{u_1}]|) +$$

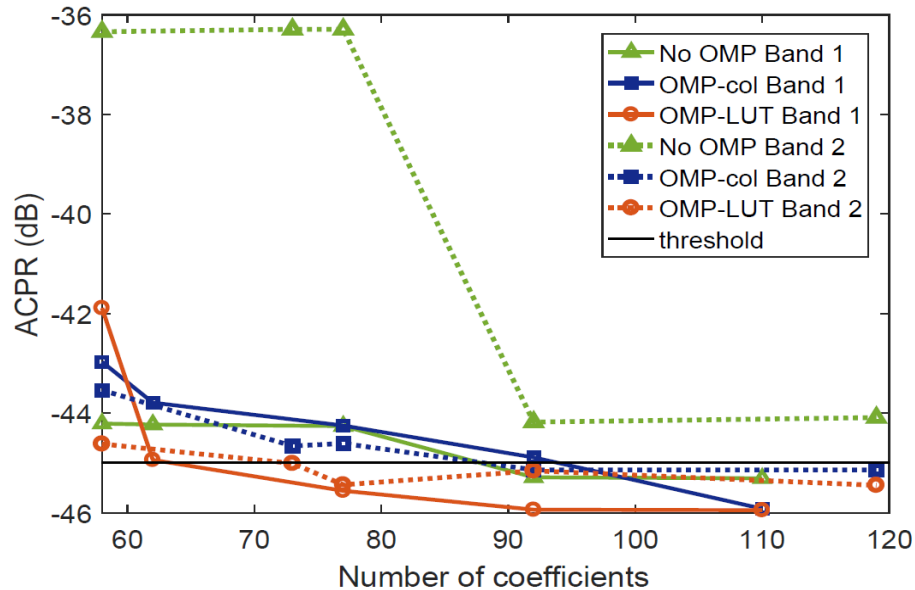
the linear combination of basis functions of linear interpolation/extrapolation, 1-D LUT.

$$\sum_{i=1}^{N_2-1} \sum_{j=1}^{M_2-1} u_1[n] f_{\Phi_{1,i,j}}(|u_1[n - \tau_i^{u_1}]|, |u_2[n - \tau_j^{u_2}]|) +$$

$$\sum_{i=1}^{N_3-1} \sum_{k=1}^{K_3-1} u_1[n] f_{\Phi_{1,i,k}}(|u_1[n - \tau_i^{u_1}]|, E[n - \tau_k^e]) +$$

the linear combination of basis functions of bilinear interpolation/extrapolation, 2-D LUT.

OMP for 3D-DPD for Concurrent DB ET PAs



Method	Pout (dBm)	η (%)	NMSE (dB)	ACPR (dB)	Num. coeff.
(a)			B1: -36,51	B1: -45,59	B1: 85
No OMP	23,1	18,97	B2: -37,67	B2: -46,02	B2: 153
(b)			B1: -36,30	B1: -45,14	B1: 92
OMP-col	22,8	18,21	B2: -37,48	B2: -45,33	B2: 92
(c)			B1: -36,50	B1: -45,05	B1: 62
OMP-LUT	23,0	18,67	B2: -37,14	B2: -45,25	B2: 73

With OMP the most relevant basis functions (or LUT coefficients) are selected \rightarrow trade-off between the number of coefficients used and the amount of non-linearity compensation.

Feature Extraction: PCA and PLS

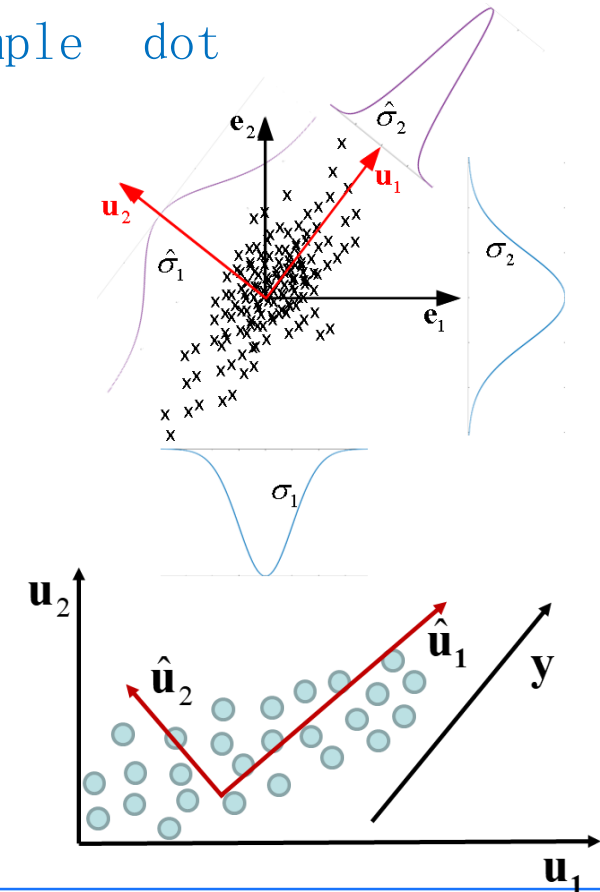
In **PCA** and **PLS**, thanks to the orthogonality of the resulting transformed matrix, the DPD coefficients' extraction can be carried out with **simple dot products** (avoiding matrix inversions).

$$\hat{\mathbf{U}}_{PCA} = \mathbf{UV}$$

The principal components are linear combinations of the original variables oriented to capture the maximum variance in the data contained in \mathbf{U} .

$$\hat{\mathbf{U}}_{PLS} = \mathbf{UT}$$

PLS generates components that capture most of the information in \mathbf{U} , that are useful for predicting \mathbf{y} .



Feature Extraction: PCA and PLS

$$\hat{\mathbf{U}}_{PCA} = \mathbf{U}\mathbf{V} \Rightarrow (\hat{\mathbf{U}}^H \hat{\mathbf{U}})^{-1} = \text{diag}(\lambda_1^{-1} \lambda_2^{-1} \mathbf{L} \lambda_N^{-1})$$

λ_i
are the eigenvalues of $\mathbf{U}^H \mathbf{U}$ (with $i=1, 2, \dots, N$)

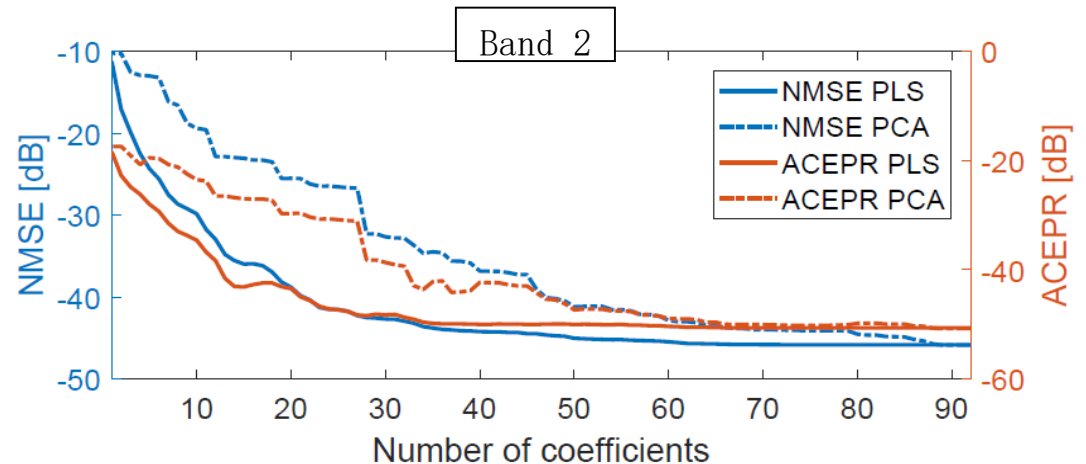
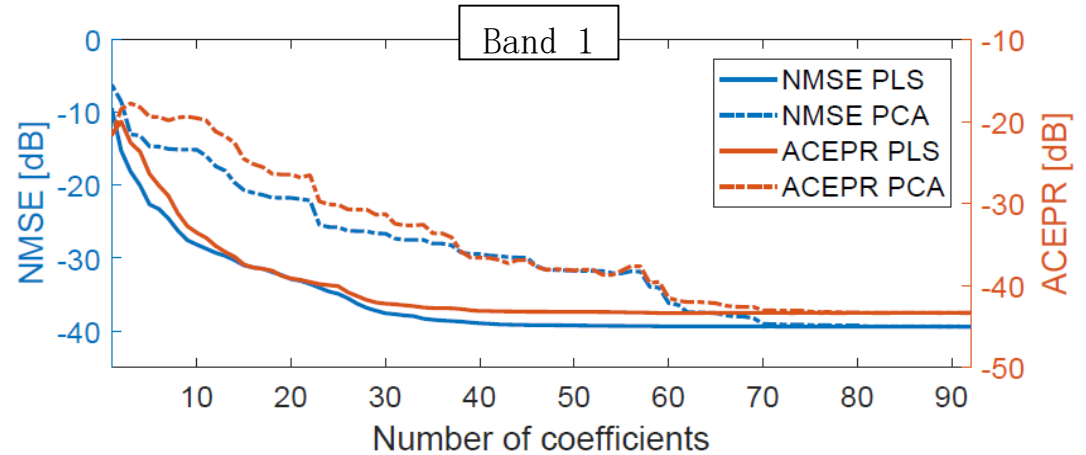
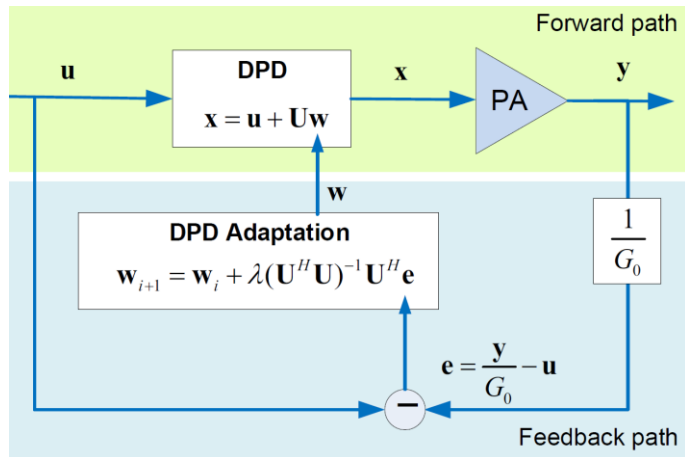
$$\hat{\mathbf{w}}_{n+1} = \hat{\mathbf{w}}_n + \mu \Delta \hat{\mathbf{w}}_n \rightarrow \begin{bmatrix} \hat{w}_1(n+1) \\ \hat{w}_2(n+1) \\ \mathbf{M} \\ \hat{w}_N(n+1) \end{bmatrix} = \begin{bmatrix} \hat{w}_1(n) \\ \hat{w}_2(n) \\ \mathbf{M} \\ \hat{w}_N(n) \end{bmatrix} + \mu \begin{bmatrix} \lambda_1^{-1} \gamma_1(n) \\ \lambda_2^{-1} \gamma_2(n) \\ \mathbf{M} \\ \lambda_N^{-1} \gamma_N(n) \end{bmatrix} e(n) \Rightarrow \mathbf{w} = \mathbf{V} \hat{\mathbf{w}}$$

$$\hat{\mathbf{U}}_{PLS} = \mathbf{U}\mathbf{T} \Rightarrow (\hat{\mathbf{U}}^H \hat{\mathbf{U}})^{-1} = \mathbf{I}$$

$$\hat{\mathbf{w}}_{n+1} = \hat{\mathbf{w}}_n + \mu \Delta \hat{\mathbf{w}}_n \rightarrow \begin{bmatrix} \hat{w}_1(n+1) \\ \hat{w}_2(n+1) \\ \mathbf{M} \\ \hat{w}_N(n+1) \end{bmatrix} = \begin{bmatrix} \hat{w}_1(n) \\ \hat{w}_2(n) \\ \mathbf{M} \\ \hat{w}_N(n) \end{bmatrix} + \mu \begin{bmatrix} \gamma_1(n) \\ \gamma_2(n) \\ \mathbf{M} \\ \gamma_N(n) \end{bmatrix} e(n) \Rightarrow \mathbf{w} = \mathbf{T} \hat{\mathbf{w}}$$

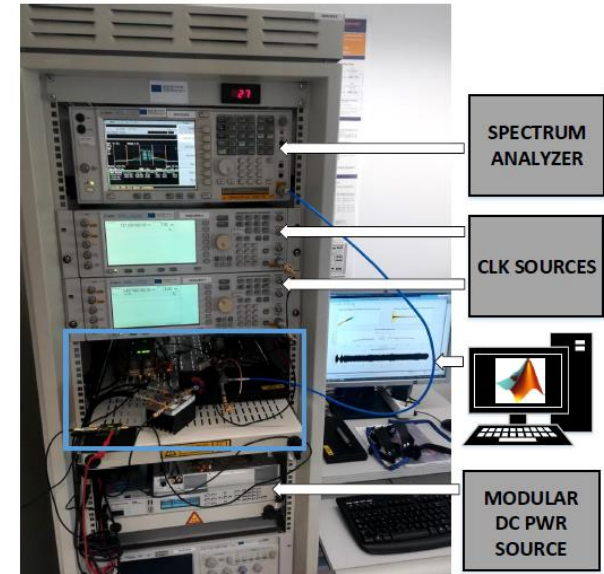
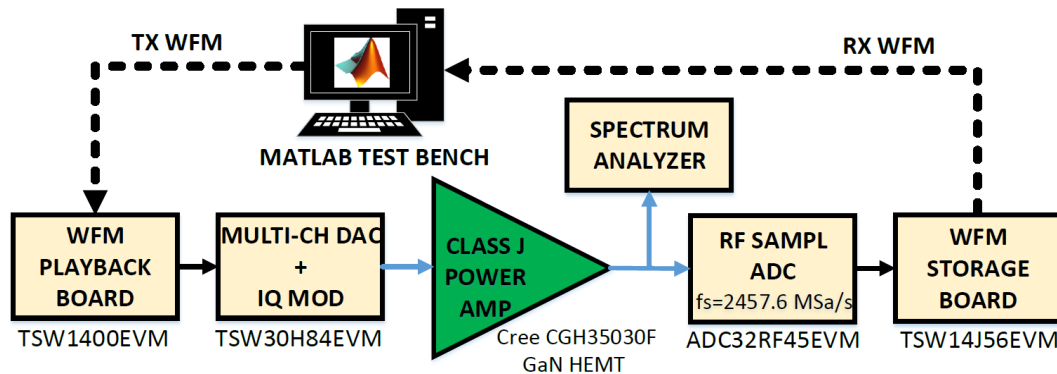
Performance Comparison between PCA and PLS

- Forward path: OMP-col
- Feedback path: PLS/PCA

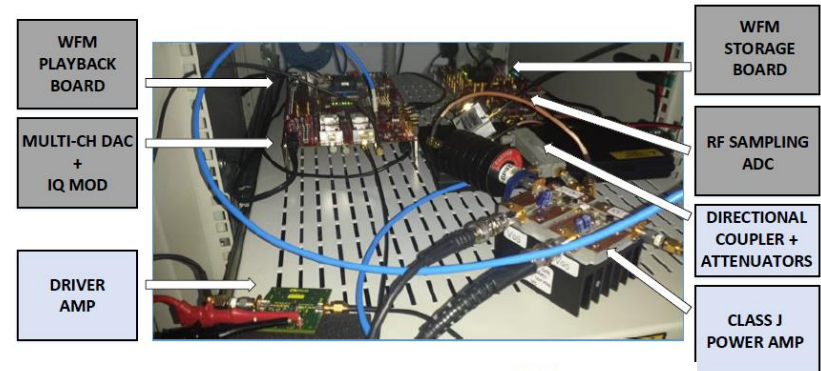


Q. A. Pham, D. Lopez-Bueno, T. Wang, G. Montoro and P. L. Gilibert, "Partial Least Squares Identification of Multi Look-up Table Digital Predistorters for Concurrent Dual-Band Envelope Tracking Power Amplifiers" submitted to T-MTT.

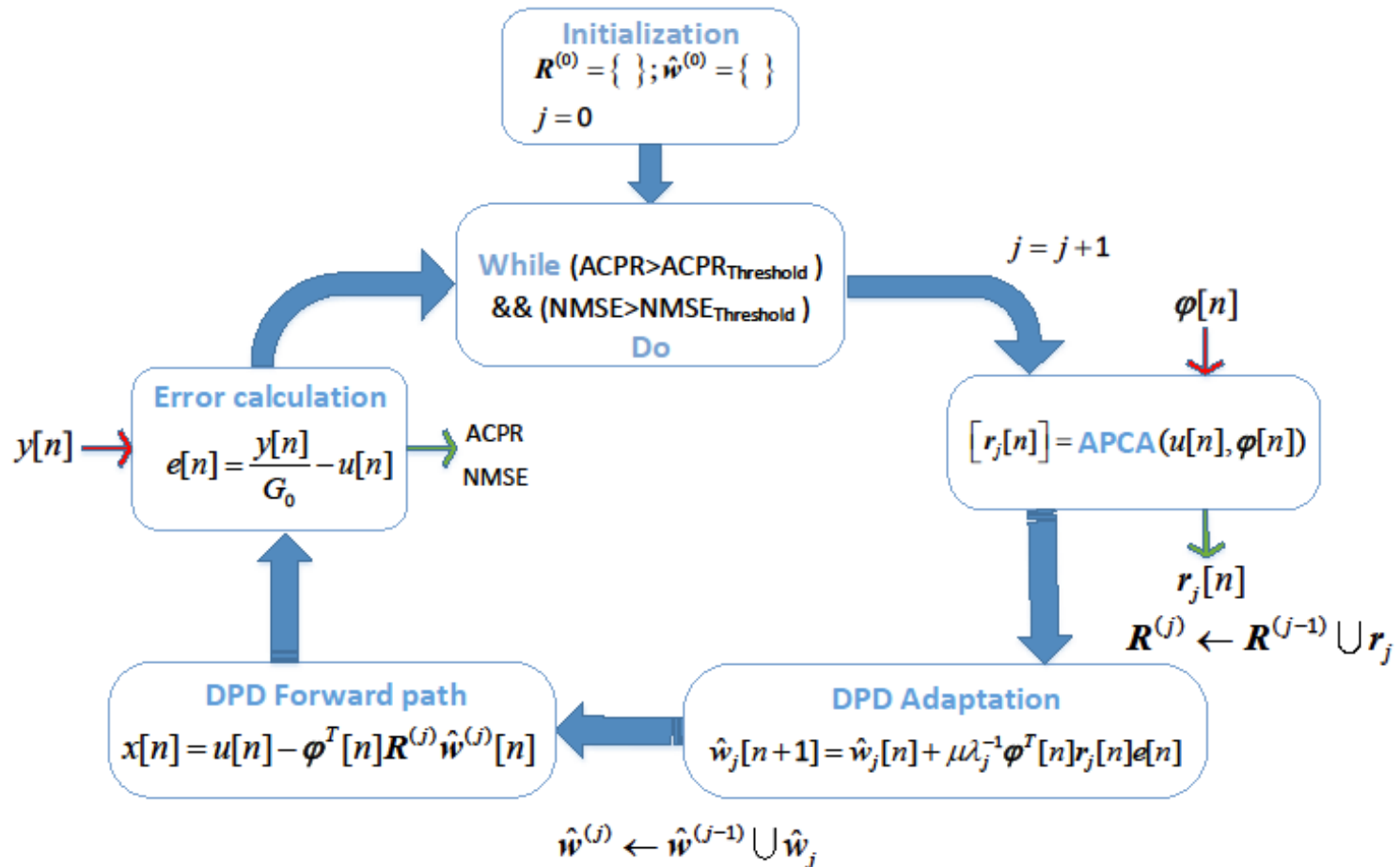
Matlab-controlled digital linearization test bench.




- Test signal: filter bank multi-carrier signal with 80 MHz bandwidth and 13 dB of PAPR.
- Mean output power: 28 dBm
- Targeted ACPR levels < -45 dB
- GMP-based DPD
- DUT: Broadband high efficiency continuous mode class-J GaN power amplifier at 875 MHz.

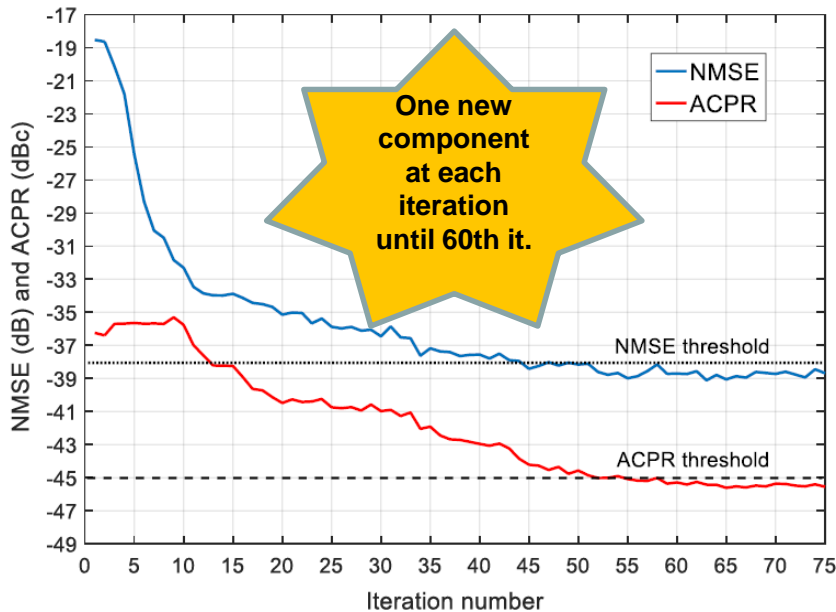


Independent DPD Adaptation using Adaptive PCA

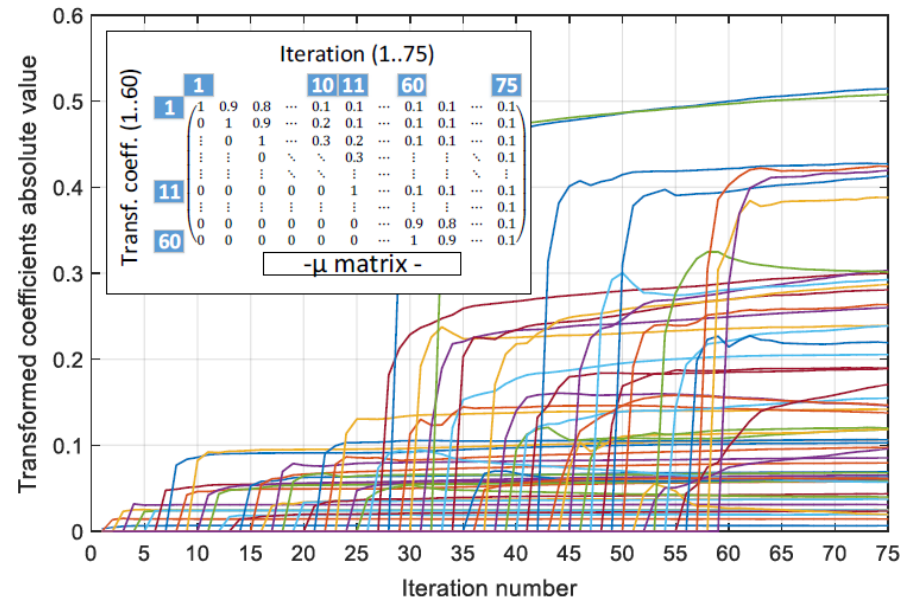



 D. Lopez, Q. A. Pham, G. Montoro, P. L. Gilibert, "Independent Digital Predistortion Parameters Estimation Using Adaptive Principal Component Analysis", *IEEE Transactions on Microwave Theory and Techniques*.


Independent DPD Adaptation using Adaptive PCA



Evolution of the NMSE and the ACPR considering 60 components and 75 iterations.



Evolution of the absolute value of the 60 DPD coefficients.

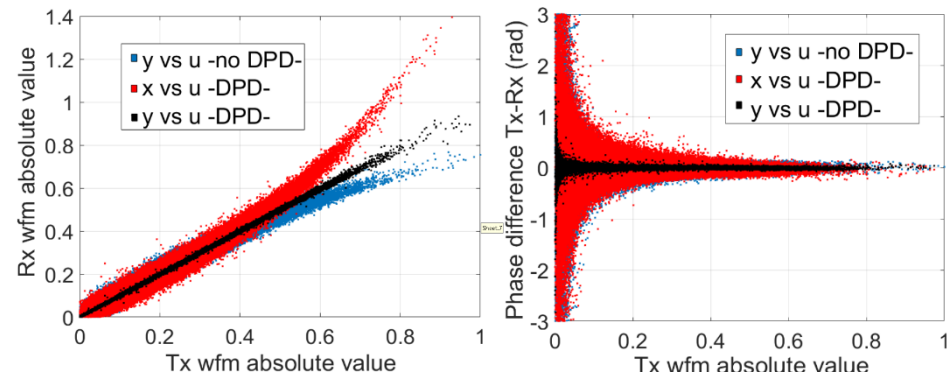
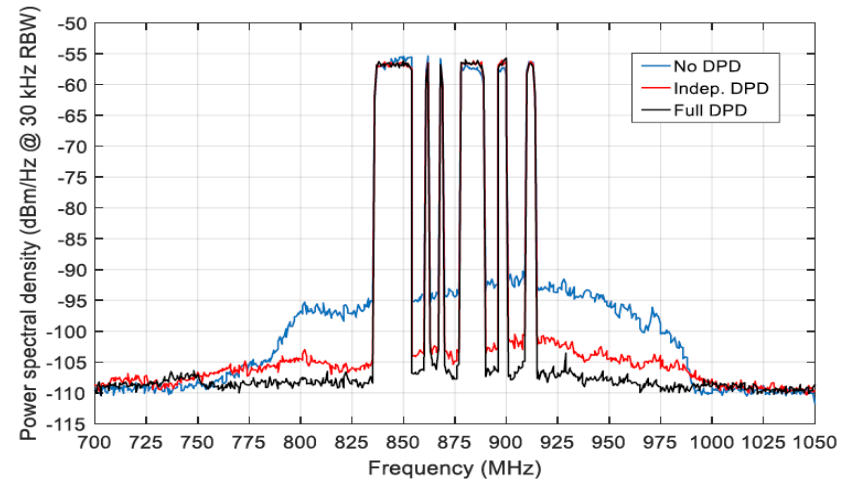

 D. Lopez, Q. A. Pham, G. Montoro, P. L. Gilibert, "Independent Digital Predistortion Parameters Estimation Using Adaptive Principal Component Analysis", *IEEE Transactions on Microwave Theory and Techniques*, vol. 66, no. 12, pp. 5771-5779, Dec. 2018.


Independent DPD Adaptation using Adaptive PCA

DPD linearization results

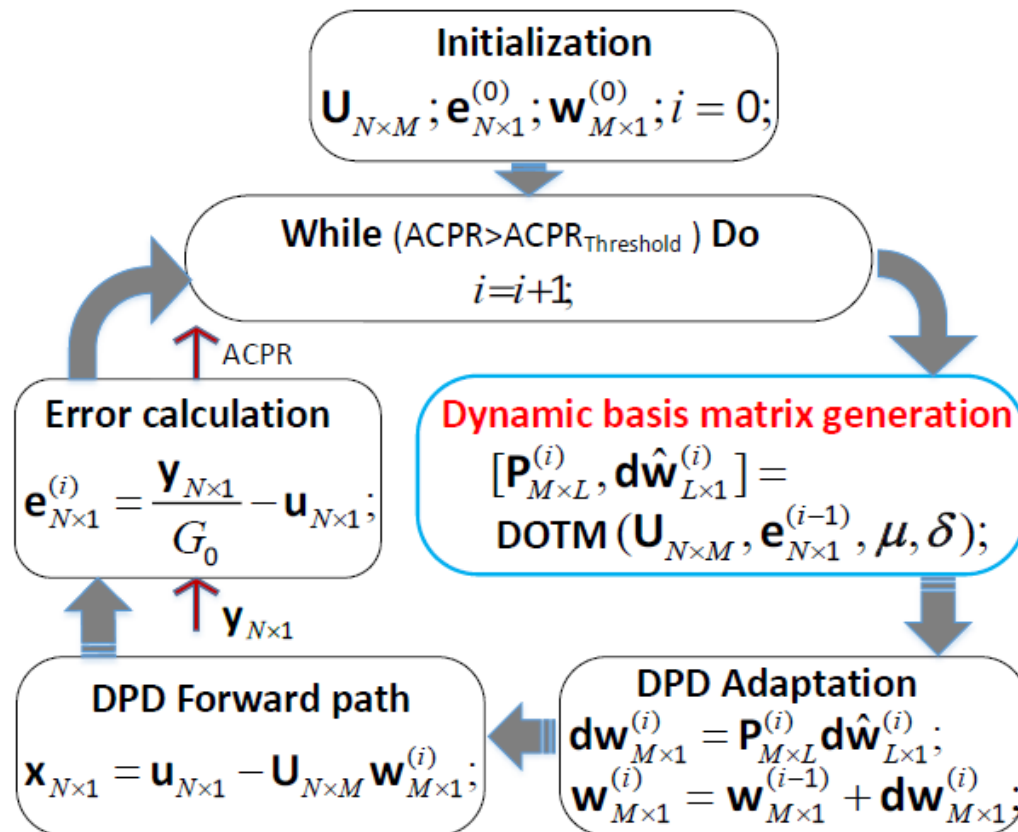
Configuration	Coeff.	NMSE	ACPR	EVM
80 MHz FC-FBMC	No.	[dB]	[dBc]	[%]
No DPD	-	-18.5	-36.25	5.75
Full DPD w/ Matlab's '\'	322	-41.1	-50.7	1.05
Indep. DPD w/ APCA	60	-38.7	-45.3	1.35

With APCA, to meet the targeted linearity specifications ($ACPR \leq -45$ dBc, $NMSE \leq -38$ dB), **only 60 coeff.** (= 19% of Full DPD) are required.




 D. Lopez, Q. A. Pham, G. Montoro, P. L. Gilabert, "Independent Digital Predistortion Parameters Estimation Using Adaptive Principal Component Analysis", *IEEE Transactions on Microwave Theory and Techniques*, vol. 66, no. 12, pp. 5771-5779, Dec. 2018.

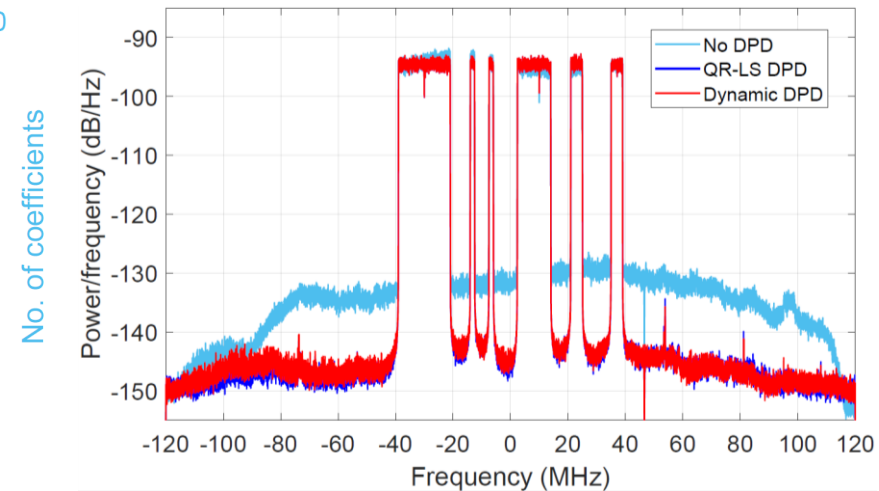
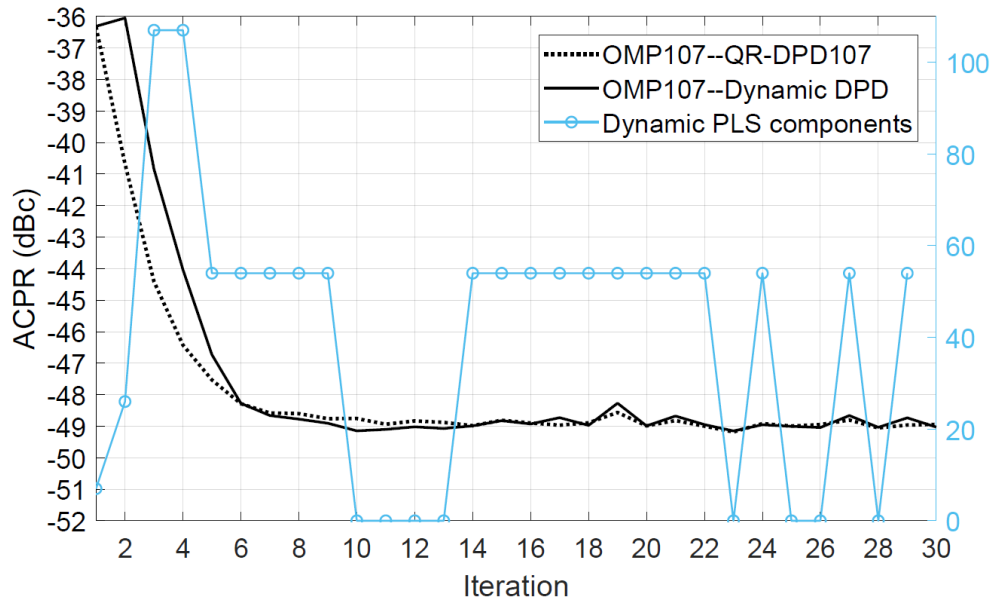
Dynamic basis selection for DPD adaptation using PLS



Dynamic Orthonormal Transformation Matrix (DOTM) alg. is a modification of the SIMPLS alg.

 Q. A. Pham, D. López-Bueno, G. Montoro, and P. L. Gilabert, "Dynamic selection and update of digital predistorter coefficients for power amplifier linearization," in *Proc. 2019 IEEE Topical Conf. on RF/Microw. Power Amplifiers for Radio and Wireless Appl. (PAWR)*, Jan. 2019, pp. 1–4.

Dynamic basis selection for DPD adaptation using PLS



The DPD estimation/adaptation with DOTM vs. with QR decomposition.

- Original basis functions: 322 coeff.
- Forward path, after OMP: 107 coeff.

- Both DPD adaptations converge after 10 iterations with same ACPR level.
- DPD with QR-LS (using Givens rotations alg.) requires 107 coeff. at every iteration.
- DPD with DOTM need less coeff. (53, 21, 5 or 1 coeff.) to achieve same ACPR.

- ❑ Introduction
- ❑ Linearity vs. Efficiency Trade-off
- ❑ High Efficient Amplification Architectures
- ❑ Digital Predistortion (DPD) Linearization
- ❑ Dimensionality Reduction Techniques
- ❑ Conclusion

- ❑ In the field of DPD linearization, **dimensionality reduction** techniques are used with a double objective:
 - Ensure a proper, **well-conditioned** parameter **identification**.
 - Reduce the number of coefficients to be estimated and thus relaxing the **computational complexity** and **memory requirements** of a hardware implementation.
- ❑ As an **alternative to QR-RLS** to solve the LS regression problem and targeting a reliable estimation we can combine:
 - an a priori **off-line search** (e.g. **OMP**) to **reduce** the number of basis functions of the DPD in the **forward path**
 - with **PLS/PCA** identification in the **adaptation path** → regularization and reduction of the number of estimated coefficients.

- ❑ In **PCA and PLS**, thanks to the orthogonality of the resulting transformed matrix, the DPD coefficients' extraction can be carried out with simple **dot products** (avoiding matrix inversions).
- ❑ **PLS shows better performance than PCA** (at the expenses of increasing the computational time) because takes into account the output data vector to compute the transformation matrix.
- ❑ Future work: **Combining PCA+PLS** → obtaining a performance equivalent to **CCA**.



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5G Technology Workshop during Mobile World Congress in Barcelona

Dimensionality Reduction Techniques for Digital Predistortion Linearization of NR- 5G Amplification Architectures

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